

10/526311  
DT01 Rec'd PCT/PT 0 2 MAR 2005

**APPLICATION FOR UNITED STATES LETTERS PATENT**

**TITLE:      IMPROVED WINDOW REGULATORY ASSEMBLY WHICH  
IS DESIGNED TO BE MOUNTED IN THE LOCK OF A  
MOTOR VEHICLE**

**INVENTOR:   Melchor DAUMAL CASTELLON**

**BLANK ROME LLP  
The Watergate  
600 New Hampshire Avenue, NW  
Washington, DC 20037  
(202) 772-5800  
(202) 572-8398 (facsimile)**

**Docket No. 001058-00023**

The present invention refers to an improved window lift assembly adapted for being fitted in the lock of a motor vehicle, which novel manufacturing, conformation and design features fulfil the purpose to which it has been specifically conceived, with a maximum safety and effectiveness, and providing many advantages as it will be herein disclosed.

More particularly, the present invention refers to the design of the window lifting device for motor vehicles of the type of those being fixed in the lock device of the motor vehicle, that is, in which the track where the window pane driving slider is fixed to the lock device of the motor vehicle. In this particular type of window lift there is provided an additional slider within the frame of the door of the motor vehicle.

The invention provides a new design of said type of window lifting devices which calculation variables are defined in such a way that the stability of the assembly, which is the main problem to be overcome in these window lifting devices, as it will be herein disclosed, is completely guaranteed, further allowing to know the feasibility of a project for a window lift assembly to be fitted in a lock device.

The above mentioned disadvantage of the window lifting devices fixed to the lock of the motor vehicle lies basically in the uncertainty of the assembly in use, which is mainly due to the fact that both fixing of the window in the slider and the guiding thereof result in backlash and interferences which negatively influences the system operation. Backlash and interferences are indeed amplified to a large extent by the action of the cantilevered pane due to the fact that the window lifting device is mounted in the lock, that is, on a side end of the door.

Practice has clearly shown that the main problem in this type of window lifting devices resides in the

difficulty of maintaining the system stable since, as outlined above, the pane may have a great length which consequently results in a high torque that makes the system unstable. In this sense, it should be especially stressed the fact that the load center, that is to say, the weight of the pane plus frictions, is located quite far from the center of thrust of the window lift driving cable.

With the aim of seeking an effective solution that allows to maintain the static and dynamic stability condition required for a window lifting device of the type of those being mounted in the lock of the door of a motor vehicle, the improved window lift assembly adapted for being fitted in the lock of a motor vehicle of the present invention has been developed, which will be herein fully described.

This window lift is, as noted above, of the type of which essentially comprises two guide and slider assemblies, one of which is fitted in the frame of the door and the other of which is fitted in the track of the window lift. It further comprises slider driving means that include an electric motor having a gearmotor. The sliders are fixed to the window pane and the assembly is mounted attached to the lock of the motor vehicle with the track secured thereto.

The invention ascertains the necessary conditions which the design variables should meet for the feasibility of a stable assembly. Said variables present in this calculation are those herein set forth:

(Y<sub>1</sub>): distance between two points of contact of the slider in the track measured on a line parallel to said track;

(Y<sub>2</sub>): distance from the upper edge of the pane to the fastening point of the slider of the door;

(X<sub>1</sub>): distance from an end of the track (which is secured to the door frame) to the points of contact of the

slider in the track;

(X<sub>2</sub>): horizontal distance between two points of contact of the slider in the track;

(H): height of the lower edge of the door of the vehicle to the belt line; and

(h): height of the window of the vehicle.

The conditions which have to be met by said variables so that the design of this window lifting device is feasible are the following:

i) (Y<sub>1</sub>) should be the maximum value possible for generating the maximum resistive torque to withstand the weight of the pane and, at the same time, the condition that (Y<sub>1</sub>) < (H-h) should be also met in order to facilitate the assembly of the slider in the door;

ii) (Y<sub>2</sub>) < (h-Y<sub>2</sub>) since the descent load is less than the ascent torque due to gravity. As the pane carries out an upward movement, the window lift should overcome friction and the weight of the pane, while as the pane carries out a downward movement, loads are friction minus the weight of the pane; and

iii) (X<sub>1</sub>) should be as high as possible according to the geometry of the door.

In the event the value (Y<sub>1</sub>) is very low, due to space reasons, and to the geometry of the door, a condition that (X<sub>2</sub>) ≤ ((X<sub>1</sub>) should be additionally met.

Preferably, (X<sub>1</sub>) is of the order of 100-150 mm, depending on the space available for assembly.

Therefore, according to the invention, it is necessary to keep in mind at least three variables (Y<sub>1</sub>, Y<sub>2</sub>, X<sub>1</sub>) in order for the assembly to be stable depending on the geometry and the loads on each door.

An increased (Y<sub>1</sub>) involves a higher limitation of rotation of the window lift slider on the track, so that

the window lift becomes stronger. On the other hand, ( $Y_2$ ,  $X_2$ ) depend on friction loads.

Regarding the design of the slider of the guide of the vehicle door, guiding inside the door frame may be carried out in three ways:

1- By only providing a single point of contact inside said guide, which allows rotation. In this case, in order to provide stability to the system, ( $Y_1$ ) should be as high as possible, ( $X_1$ ) should be as low as possible and ( $Y_2$ ) depends on the load.

2- Completely guided without possibility of rotation. In this case ( $Y_1$ ) should be as low as possible to avoid hyperstability and to prevent the system from being blocked, and ( $X_1$ ) should be also as low as possible to avoid any possible blocking torques.

3- The slider will have a single point of contact as in the first case, but the pane completely rests on the door frame. In this case ( $Y_1$ ,  $Y_2$ ,  $X_1$ ) should be calculated according to geometry and loads, without considering maximum and minimum values. ( $Y_1$ ) should be an average value to avoid possible plays in the system, while ( $Y_2$ ,  $X_2$ ) should be proportional to ascent and descent loads.

The sliders used in the window lift described according to the present invention are made preferably, but not exclusively, of carbon fiber and combinations thereof with POM, PP66 or other similar plastic materials suitable for this purpose with the addition of materials for promoting slippage and reducing the abrasive nature of the carbon fiber. With the choice of these materials it is possible to obtain sliders which are up to ten times more resistant than the conventional sliders made of POM and the like. Also, the carbon fiber allows reducing noise in use with regard to other materials typically employed for the same purpose.

A further important feature of the present

invention is the mechanical link between the window lift driving means and the lock device of the motor vehicle where it is mounted. Operation of locks in motor vehicles currently involves the use of several electric motors for driving the central locking system and other related devices. The invention proposes the mechanical connection of the window lift driving means with at least some of said devices associated with the lock assembly with the purpose of suppressing at least one of the motors used. In this sense, it should be especially stressed the fact that the feasibility of the mechanical transmission of, for example, the central locking system of a vehicle through the motor of the window lift fixed to the lock thereof is possible thanks to the high gear ration existing between the electric motor output shaft and a screw shaft meshed therewith which would act on the lock mechanism, which may be of the order of 1/70.

More particularly, if the following design variables are taken into consideration in calculation of the window lift driving means:

$\alpha_1$  = arch rotated by the drum. It equals the travel of the driving cable and the length of the pane that is moved;

$r$  = radius of the drum around which the driving cable is wound;

$\beta_1$  = angle rotated by the cable drum (in radians);

$\alpha_2$  = arch rotated by the electric motor before reduction;

$\beta_2$  = angle rotated by the electric motor before the reduction (in radians);

$Re$  = gear ration of the gearmotor between the drum axis and the electric motor output shaft;

it is provided that

$\alpha_1 = \beta_1 \cdot r$

and as  $Re = \frac{\beta_2}{\beta_1}$ , then:

$$\beta_1 = \frac{\beta_2}{Re}$$

5 Therefore, as

$$\alpha_1 = \beta_1 \cdot r$$

Then:

10 
$$\alpha_1 = \frac{\beta_2 \cdot r}{Re}$$

Replacing the variables with typical values in a window lift as in the present invention:

15 
$$r = 5\text{mm}$$

$$Re = 70$$

$$\alpha_1 = \frac{\beta_2 \cdot r}{Re} = \frac{\beta_2 \cdot 25}{70}$$

20 and expressed in degrees:

$$\alpha_1 = \frac{\beta_2 \cdot 25 \cdot \pi}{70 \cdot 180} = 0,0062333 \cdot \beta_2$$

$$\alpha_1 = \frac{\beta_2}{160,427} \Rightarrow \beta_2 = 160,427 \cdot \alpha_1 \quad (\text{in mm})$$

25 That is to say, if the travel length of the pane driving cable is 0,5 m, the electric motor rotates approximately 80°, so that there is an available energy for a mechanism like the lock device (and related mechanisms thereof) that requires a low amount of energy and this does  
30 not involve any discernable movements in the window lift. A

displacement of 0,5 mm in the drum around which the window lift driving cable is wound is hardly appreciated since there are other factors as the compression of springs, cable, rubbers, etc. before the pane is moved.

5           The design proposed in the present invention provides many advantages:

- an accurate feasibility study of the window lift for determining stability in use according to the defined variables is thus made possible;

10           - the use of a window lifting device directly fitted to the lock of the door allows the free room inside the door to be increased;

- the configuration of the window lift driving means according to the present invention allows at least  
15 one of the motors associated with the activation of the vehicle lock to be suppressed;

- a window lifting device designed according to the parameters of the present invention allows large sized and high weighted panes to be driven without problems.

20           A preferred embodiment of a window lift assembly according to the present invention is now described in detail and by way of a non limitative example, from which the features and the advantages of the invention will be clearly understood. The description that follows is given  
25 with reference to the drawing that is herein accompanied which corresponds to a diagrammatic elevational view of a vehicle door having a window lifting device according to the invention, said door being part-way shown cut so that the assembly of guides and sliders as well as the window  
30 pane are clearly seen.

The embodiment that is herein described according to the enclosed drawing is an effective solution that makes possible the condition of static and dynamic stability required for a window lift fitted in the lock of the motor  
35 vehicle door is met.



In the drawing, a door (1) of a vehicle is shown with the frame (2) where the pane (3) slides. The window lift includes a first guide and slider assembly (4) in the frame (2) of the door (1) and a second guide and slider assembly (5) in the track (6) of the window lift.

The window lift is driven through an electric motor and a gearmotor (not shown).

The slider (7) is fixed to the lower edge (8) of the pane (3) at the fastening points (10), the assembly being mounted fixed to the door lock (1) with the track (6) secured thereto.

The slider (7) is made of carbon fiber and combinations thereof with POM, PP66 or other similar plastic materials suitable for this purpose with the addition of materials for promoting slippage and reducing the abrasive nature of the carbon fiber. Carbon fiber is preferred due to its low noise in use regarding other conventional materials.

The feasibility of this window lift assembly depends on at least three variables ( $Y_1$ ,  $Y_2$ ,  $X_1$ ) which are a function of the geometry and the loads on each door.

Variable ( $Y_1$ ) corresponds to the distance between two points of contact (P) of the slider (7) in the track (6) measured on a line parallel to said track (6). Variable ( $Y_2$ ) is the distance from the upper edge (11) of the pane (3) to the fastening point (12) of the slider (4) running through the length (9) of the frame (2) of the door (1). The third design variable ( $X_1$ ) is the distance from an end of the track (6) -which is secured to the frame (2) of the door (1)- to the points of contact (P) of the slider (7) in the track (6).

A fourth additional variable called ( $X_2$ ) may be defined corresponding to the horizontal distance between two points of contact (P) of the slider (7) in the track (6).

Other values to be taken into consideration are the height (H) from the lower portion (14) of the door (1) of the vehicle to the belt line (13); and the height (h) of the window of the vehicle.

5           According to the invention, in order the design of said window lift is made feasible, the condition that ( $Y_1$ ) is the maximum value possible for generating the maximum resistive torque to withstand the weight of the pane (3) should be met and, at the same time, the condition  
10 that ( $Y_1$ ) < (H-h) should be also met to facilitate the assembly of the slider (7) in the door. It should be also met that ( $Y_2$ ) is less than the value (h- $Y_2$ ) since the descent load is less than the ascent torque due to gravity. As the pane (3) carries out an upward movement, the window  
15 lift should overcome friction as well as the weight of the pane (3), while as the pane (3) carries out a downward movement, loads are friction minus the weight of the pane(3). Finally, distance ( $X_1$ ) should be as greater as possible according to the geometry of the door (1).

20           If distance ( $Y_1$ ) is very low, due to space reasons, and to the geometry of the door (1), an additional condition that distance ( $X_2$ ) is less than or equal to ( $X_1$ ) should be additionally met, the latter being of the order of 100-150 mm, depending on the space  
25 available for assembly.

          The increase of distance ( $Y_1$ ) involves a greater limitation of rotation of the slider (7) of the window lift on the track (6), so that the window lift becomes stronger. On the other hand, distances ( $Y_2$ ,  $X_2$ ) depend on friction  
30 loads.

          Regarding the design of the slider (4) of the door guide (1) of the vehicle, guiding inside the frame (2) of the door (1) may be carried out only providing a single point of contact inside the guide so that rotation is  
35 allowed. In this case, to provide stability to the system,

distance ( $Y_1$ ) should be as high as possible, ( $X_1$ ) should be as low as possible, ( $Y_2$ ) being load dependant.

Guiding inside the frame (2) of the door (1) may be alternatively carried out without possibility of rotation, in which case, distance ( $Y_1$ ) then should be as low as possible to avoid hyperstability and to prevent the system from being blocked, distance ( $X_1$ ) then being as low as possible to avoid any possible blocking torques.

Finally, guiding inside the frame (2) of the door (1) may be also carried out according to the invention by providing a single point of contact as in the first case, but with the pane (3) completely resting on the frame (2) of the door (1). In this case ( $Y_1$ ,  $Y_2$ ,  $X_1$ ) should be calculated according to the geometry and the loads, without considering maximum and minimum values. ( $Y_1$ ) should be an average value to avoid possible plays in the system, while ( $Y_2$ ,  $X_2$ ) should be proportional to ascent and descent loads.

Once having been sufficiently described what the present invention consists according to the enclosed drawing, it is understood that any detail modification can be introduced as appropriate, provided that variations may alter the essence of the invention as summarised in the appended claims.